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Sheet Metal Operations Formulas

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List of 26 Sheet Metal Operations Formulas

Sheet Metal Operations

Bending Operation

1) Bend Allowance

$$fx \quad B_{al} = \theta \cdot (r_c + \lambda \cdot t_{bar})$$

Open Calculator 

$$ex \quad 0.026125mm = 3.14rad \cdot (0.007mm + 0.44 \cdot 0.003mm)$$

2) Bending Force

$$fx \quad F_B = \frac{K_{bd} \cdot L_b \cdot \sigma_{ut} \cdot t_{blank}^2}{w}$$

Open Calculator 

$$ex \quad 32.5425N = \frac{0.031 \cdot 1.01mm \cdot 450N/mm^2 \cdot (8.99mm)^2}{34.991620mm}$$

3) Clearance between Two Shears

$$fx \quad C_s = 0.0032 \cdot t_b \cdot (\tau)^{0.5}$$

Open Calculator 

$$ex \quad 51.13796mm = 0.0032 \cdot 1.13mm \cdot (200N/mm^2)^{0.5}$$



4) Length of Bent Part in Bending Operation

$$\text{fx } L_b = \frac{F_B \cdot w}{K_{bd} \cdot \sigma_{ut} \cdot t_{stk}^2}$$

[Open Calculator !\[\]\(cbe80b694ebd74fcfe136a095b608235_img.jpg\)](#)

$$\text{ex } 1.007757\text{mm} = \frac{32.5425\text{N} \cdot 34.991620\text{mm}}{0.031 \cdot 450\text{N/mm}^2 \cdot (9\text{mm})^2}$$

5) Stock Thickness used in Bending Operation

$$\text{fx } t_{stk} = \sqrt{\frac{F_B \cdot w}{K_{bd} \cdot L_b \cdot \sigma_{ut}}}$$

[Open Calculator !\[\]\(3e2231b1ad3ca8da8658228c00dd08e0_img.jpg\)](#)

$$\text{ex } 8.99\text{mm} = \sqrt{\frac{32.5425\text{N} \cdot 34.991620\text{mm}}{0.031 \cdot 1.01\text{mm} \cdot 450\text{N/mm}^2}}$$

6) Width between Contact Points during Bending

$$\text{fx } w = \frac{K_{bd} \cdot L_b \cdot \sigma_{ut} \cdot t_{blank}^2}{F_B}$$

[Open Calculator !\[\]\(0d5ec72f61334709c3fc9450209b754f_img.jpg\)](#)

$$\text{ex } 34.99162\text{mm} = \frac{0.031 \cdot 1.01\text{mm} \cdot 450\text{N/mm}^2 \cdot (8.99\text{mm})^2}{32.5425\text{N}}$$



Drawing Operation

7) Blank Diameter from Percent Reduction

$$\text{fx } D_b = d_s \cdot \left(1 - \frac{\text{PR}_{\%}}{100}\right)^{-1}$$

[Open Calculator !\[\]\(23d9fc146e83b5c3013cfa32c784f8d5_img.jpg\)](#)

$$\text{ex } 84.21053\text{mm} = 80\text{mm} \cdot \left(1 - \frac{5}{100}\right)^{-1}$$

8) Blank Size for Drawing Operation

$$\text{fx } D_b = \sqrt{d_s^2 + 4 \cdot d_s \cdot h_{\text{shl}}}$$

[Open Calculator !\[\]\(aa53ad6fea213b8b2226d3077e30533a_img.jpg\)](#)

$$\text{ex } 84.19026\text{mm} = \sqrt{(80\text{mm})^2 + 4 \cdot 80\text{mm} \cdot 2.15\text{mm}}$$

9) Drawing Force for Cylindrical Shells

$$\text{fx } P_d = \pi \cdot d_s \cdot t_b \cdot \sigma_y \cdot \left(\frac{D_b}{d_s} - C_f\right)$$

[Open Calculator !\[\]\(626ce8ac21792b9405bfddfea8e0c96a_img.jpg\)](#)

$$\text{ex } 0.004498\text{N/mm}^2 = \pi \cdot 80\text{mm} \cdot 1.13\text{mm} \cdot 35\text{N/mm}^2 \cdot \left(\frac{84.2\text{mm}}{80\text{mm}} - 0.6\right)$$



10) Percent Reduction after Drawing

$$fx \quad PR_{\%} = 100 \cdot \left(1 - \frac{d_s}{D_b} \right)$$

[Open Calculator !\[\]\(e2376d476d06eb31946dc01a69a4403a_img.jpg\)](#)

$$ex \quad 4.988124 = 100 \cdot \left(1 - \frac{80\text{mm}}{84.2\text{mm}} \right)$$

11) Shell Diameter from Percent Reduction

$$fx \quad d_s = D_b \cdot \left(1 - \frac{PR_{\%}}{100} \right)$$

[Open Calculator !\[\]\(0b5e7e25e8775f7e7e80906ada4f0021_img.jpg\)](#)

$$ex \quad 79.99\text{mm} = 84.2\text{mm} \cdot \left(1 - \frac{5}{100} \right)$$

Ironing Operation

12) Average of Tensile Strength before and after Ironing

$$fx \quad S_{avg} = \frac{F}{\pi \cdot d_1 \cdot t_f \cdot \ln\left(\frac{t_0}{t_f}\right)}$$

[Open Calculator !\[\]\(0fb13ad0bfa3d86868cdd3883e5665b3_img.jpg\)](#)

$$ex \quad 0.181902\text{N/mm}^2 = \frac{8.01\text{N}}{\pi \cdot 2.5\text{mm} \cdot 13\text{mm} \cdot \ln\left(\frac{20.01\text{mm}}{13\text{mm}}\right)}$$



13) Ironing Force after Drawing

[Open Calculator !\[\]\(eafc244b53721dd1ec133f0772f70fc7_img.jpg\)](#)

$$fx \quad F = \pi \cdot d_1 \cdot t_f \cdot S_{avg} \cdot \ln\left(\frac{t_0}{t_f}\right)$$

$$ex \quad 8.009301N = \pi \cdot 2.5mm \cdot 13mm \cdot 0.181886N/mm^2 \cdot \ln\left(\frac{20.01mm}{13mm}\right)$$

14) Mean Diameter of Shell after Ironing

[Open Calculator !\[\]\(10f8862fc183b400327470ea85afe9ae_img.jpg\)](#)

$$fx \quad d_1 = \frac{F}{\pi \cdot S_{avg} \cdot t_f \cdot \ln\left(\frac{t_0}{t_f}\right)}$$

$$ex \quad 2.500218mm = \frac{8.01N}{\pi \cdot 0.181886N/mm^2 \cdot 13mm \cdot \ln\left(\frac{20.01mm}{13mm}\right)}$$

15) Thickness of Shell before Ironing

[Open Calculator !\[\]\(35dc653d59570f8f891c312eeece91a2_img.jpg\)](#)

$$fx \quad t_0 = t_f \cdot \exp\left(\frac{F}{\pi \cdot d_1 \cdot t_f \cdot S_{avg}}\right)$$

$$ex \quad 20.01075mm = 13mm \cdot \exp\left(\frac{8.01N}{\pi \cdot 2.5mm \cdot 13mm \cdot 0.181886N/mm^2}\right)$$



Punch Operation

16) Blank Size when there is Corner Radius on Punch

$$fx \quad d_{bl} = \sqrt{d_s^2 + 4 \cdot d_s \cdot h_{shl} - 0.5 \cdot r_{cn}}$$

[Open Calculator !\[\]\(83f22ed94ec5517769dd76d702c6bfd8_img.jpg\)](#)

ex

$$84.18135\text{mm} = \sqrt{(80\text{mm})^2 + 4 \cdot 80\text{mm} \cdot 2.15\text{mm} - 0.5 \cdot 0.003001\text{mm}}$$

17) Maximum Shear Force given Shear Applied to Punch or Die

$$fx \quad F_s = L_{ct} \cdot t_{stk} \cdot \frac{t_{stk} \cdot p}{t_{sh}}$$

[Open Calculator !\[\]\(d0262bbe9d2356661a2e89321dfcc781_img.jpg\)](#)

$$ex \quad 0.015584\text{N} = 615.66\text{m} \cdot 9\text{mm} \cdot \frac{9\text{mm} \cdot 0.499985\text{mm}}{1.599984\text{mm}}$$

18) Penetration of Punch as Fraction

$$fx \quad p = \frac{F_s \cdot t_{sh}}{L_{ct} \cdot t_{stk}^2}$$

[Open Calculator !\[\]\(274fd520e03b61c1b9ffc861754cacdc_img.jpg\)](#)

$$ex \quad 0.499581\text{mm} = \frac{0.015571\text{N} \cdot 1.599984\text{mm}}{615.66\text{m} \cdot (9\text{mm})^2}$$



19) Perimeter of Cut when Shear is Applied

$$fx \quad L_{ct} = \frac{F_s \cdot t_{sh}}{p \cdot t_{stk}^2}$$

[Open Calculator !\[\]\(6605b201d6f14d9b3bcb8ab5f274d107_img.jpg\)](#)

$$ex \quad 615.1629m = \frac{0.015571N \cdot 1.599984mm}{0.499985mm \cdot (9mm)^2}$$

20) Punch Load

$$fx \quad L_p = L_{ct} \cdot t_{bar} \cdot S_c$$

[Open Calculator !\[\]\(e8fb589d58dad1692debababa5e928b6_img.jpg\)](#)

$$ex \quad 16.83061N = 615.66m \cdot 0.003mm \cdot 9112.5$$

21) Punching Force for Holes Smaller than Sheet Thickness

$$fx \quad P = \frac{d_{rm} \cdot t_b \cdot \varepsilon}{\left(\frac{d_{rm}}{t_b}\right)^{\frac{1}{3}}}$$

[Open Calculator !\[\]\(4688aadfd656ded00cd6bdfae55089a9_img.jpg\)](#)

$$ex \quad 178.3896N = \frac{13.3mm \cdot 1.13mm \cdot 27N/mm^2}{\left(\frac{13.3mm}{1.13mm}\right)^{\frac{1}{3}}}$$

22) Shear on Punch or Die

$$fx \quad t_{sh} = L_{ct} \cdot t_{stk} \cdot \frac{t_{stk} \cdot p}{F_s}$$

[Open Calculator !\[\]\(4146d17f71dced09c6ad789cacceaa6d_img.jpg\)](#)


$$ex \quad 1.601277mm = 615.66m \cdot 9mm \cdot \frac{9mm \cdot 0.499985mm}{0.015571N}$$



23) Stock Thickness when Shear used on Punch Open Calculator 


$$fx \quad t_{stk} = \sqrt{\frac{F_s \cdot t_{sh}}{L_{ct} \cdot p}}$$

$$ex \quad 8.996366mm = \sqrt{\frac{0.015571N \cdot 1.599984mm}{615.66m \cdot 0.499985mm}}$$

Stripping Operation 24) Perimeter of Cut given Stripper Force Open Calculator 


$$fx \quad L_{cut} = \frac{P_s}{K \cdot t_{blank}}$$

$$ex \quad 617.3526mm = \frac{0.000111N}{0.02 \cdot 8.99mm}$$

25) Stripping Force Open Calculator 

$$fx \quad P_s = K \cdot L_{cut} \cdot t_{blank}$$

$$ex \quad 0.000111N = 0.02 \cdot 616.6667mm \cdot 8.99mm$$

26) Thickness of Stock given Stripper Force Open Calculator 

$$fx \quad t_{blank} = \frac{P_s}{K \cdot L_{cut}}$$

$$ex \quad 9mm = \frac{0.000111N}{0.02 \cdot 616.6667mm}$$



Variables Used





- B_{al} Bend Allowance (Millimeter)
- C_f Cover Friction Constant
- C_s Clearance between Two Shears (Millimeter)
- d_1 Mean Shell Diameter after Ironing (Millimeter)
- D_b Sheet Diameter (Millimeter)
- d_{bl} Blank Diameter (Millimeter)
- d_{rm} Punch or Ram Diameter (Millimeter)
- d_s Outer Diameter of Shell (Millimeter)
- F Ironing Force (Newton)
- F_B Bending Force (Newton)
- F_s Maximum Shear Force (Newton)
- h_{shl} Shell Height (Millimeter)
- K Stripping Constant
- K_{bd} Bending Die Constant
- L_b Bent Part Length (Millimeter)
- L_{ct} Cutting Perimeter (Meter)
- L_{cut} Perimeter of Cut (Millimeter)
- L_p Punch Load (Newton)
- p Punch Penetration (Millimeter)
- P Punching Force or Load (Newton)
- P_d Drawing Force (Newton per Square Millimeter)



- P_s Stripper Force (Newton)
- $PR\%$ Percent Reduction after Drawing
- r_c Radius (Millimeter)
- r_{cn} Corner Radius on Punch (Millimeter)
- S_{avg} Average Tensile Strength Before & After Ironing (Newton per Square Millimeter)
- S_c Strength Coefficient
- t_0 Shell Thickness before Ironing (Millimeter)
- t_b Sheet Thickness (Millimeter)
- t_{bar} Bar Thickness (Millimeter)
- t_{blank} Blank Thickness (Millimeter)
- t_f Shell Thickness after Ironing (Millimeter)
- t_{sh} Shear on Punch (Millimeter)
- t_{stk} Thickness of Stock (Millimeter)
- w Width between Contact Points (Millimeter)
- ϵ Tensile Strength (Newton per Square Millimeter)
- θ Subtended Angle in Radians (Radian)
- λ Stretch Factor
- σ_{ut} Ultimate Tensile Strength (Newton per Square Millimeter)
- σ_y Yield Strength (Newton per Square Millimeter)
- T Shear Strength of Material (Newton per Square Millimeter)



Constants, Functions, Measurements used

- **Constant:** **pi**, 3.14159265358979323846264338327950288
Archimedes' constant
- **Function:** **exp**, exp(Number)
n an exponential function, the value of the function changes by a constant factor for every unit change in the independent variable.
- **Function:** **ln**, ln(Number)
The natural logarithm, also known as the logarithm to the base e, is the inverse function of the natural exponential function.
- **Function:** **sqrt**, sqrt(Number)
A square root function is a function that takes a non-negative number as an input and returns the square root of the given input number.
- **Measurement:** **Length** in Millimeter (mm), Meter (m)
Length Unit Conversion 
- **Measurement:** **Pressure** in Newton per Square Millimeter (N/mm²)
Pressure Unit Conversion 
- **Measurement:** **Force** in Newton (N)
Force Unit Conversion 
- **Measurement:** **Angle** in Radian (rad)
Angle Unit Conversion 



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