



Power Screws Formulas

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List of 103 Power Screws Formulas

Power Screws 🕑

Acme Thread 🕑

1) Coefficient of Friction of Power Screw given Effort in Lowering Load with Acme Threaded Screw

2) Coefficient of Friction of Power Screw given Effort in Moving Load with Acme Threaded Screw

$$f_{\mathbf{X}} \mu = \frac{P_{li} - W \cdot \tan(\alpha)}{\sec\left(14.5 \cdot \frac{\pi}{180}\right) \cdot (W + P_{li} \cdot \tan(\alpha))}$$

$$e_{\mathbf{X}} 0.149953 = \frac{402N - 1700N \cdot \tan(4.5^{\circ})}{\sec\left(14.5 \cdot \frac{\pi}{180}\right) \cdot (1700N + 402N \cdot \tan(4.5^{\circ}))}$$

3) Coefficient of Friction of Power Screw given Torque Required in Lifting Load with Acme Thread

$$f_{\mathbf{X}} \mu = \frac{2 \cdot Mt_{li} - W \cdot d_{m} \cdot tan(\alpha)}{\sec(0.253) \cdot (W \cdot d_{m} + 2 \cdot Mt_{li} \cdot tan(\alpha))}$$

$$e_{\mathbf{X}} 0.150412 = \frac{2 \cdot 9265N^{*}mm - 1700N \cdot 46mm \cdot tan(4.5^{\circ})}{\sec(0.253) \cdot (1700N \cdot 46mm + 2 \cdot 9265N^{*}mm \cdot tan(4.5^{\circ}))}$$

4) Coefficient of Friction of Power Screw given Torque Required in Lowering Load with Acme Thread

fx
$$\mu = rac{2 \cdot \mathrm{Mt_{lo}} + \mathrm{W} \cdot \mathrm{d_m} \cdot \mathrm{tan}(lpha)}{\mathrm{sec}(0.253) \cdot (\mathrm{W} \cdot \mathrm{d_m} - 2 \cdot \mathrm{Mt_{lo}} \cdot \mathrm{tan}(lpha))}$$

ex
$$0.150386 = \frac{2 \cdot 2960 \text{N*mm} + 1700 \text{N} \cdot 46 \text{mm} \cdot \tan(4.5^{\circ})}{\sec(0.253) \cdot (1700 \text{N} \cdot 46 \text{mm} - 2 \cdot 2960 \text{N*mm} \cdot \tan(4.5^{\circ}))}$$

5) Efficiency of Acme Threaded Power Screw 🕑

$$\eta = an(lpha) \cdot rac{1 - \mu \cdot an(lpha) \cdot ext{sec}(0.253)}{\mu \cdot ext{sec}(0.253) + an(lpha)}$$

$$\textbf{ex} \ 0.332752 = \tan(4.5°) \cdot \frac{1 - 0.15 \cdot \tan(4.5°) \cdot \sec(0.253)}{0.15 \cdot \sec(0.253) + \tan(4.5°)}$$

6) Effort Required in Lifting Load with Acme Threaded Screw

$$\mathbf{x} \left[\mathrm{P}_{\mathrm{li}} = \mathrm{W} \cdot \left(rac{\mu \cdot \mathrm{sec}((0.253)) + \mathrm{tan}(lpha)}{1 - \mu \cdot \mathrm{sec}((0.253)) \cdot \mathrm{tan}(lpha)}
ight)
ight]$$

$$\textbf{ex} \ 402.0803 \text{N} = 1700 \text{N} \cdot \left(\frac{0.15 \cdot \sec((0.253)) + \tan(4.5\degree)}{1 - 0.15 \cdot \sec((0.253)) \cdot \tan(4.5\degree)} \right)$$

7) Effort Required in Lowering Load with Acme Threaded Screw C

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$$\mathrm{P}_{\mathrm{lo}} = \mathrm{W} \cdot \left(rac{\mu \cdot \mathrm{sec}((0.253)) - \mathrm{tan}(lpha)}{1 + \mu \cdot \mathrm{sec}((0.253)) \cdot \mathrm{tan}(lpha)}
ight)$$

fx

f

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Open Calculator 🕑

Open Calculator

8) Helix Angle of Power Screw given Effort Required in Lifting Load with Acme Threaded Screw

$$lpha = a aniggl(rac{ ext{P}_{ ext{li}} - ext{W} \cdot \mu \cdot ext{sec}(0.253)}{ ext{W} + ext{P}_{ ext{li}} \cdot \mu \cdot ext{sec}(0.253)} iggr)$$

$$4.497438^{\circ} = a \tan \left(\frac{402\mathrm{N} - 1700\mathrm{N} \cdot 0.15 \cdot \mathrm{sec}(0.253)}{1700\mathrm{N} + 402\mathrm{N} \cdot 0.15 \cdot \mathrm{sec}(0.253)} \right)$$

9) Helix Angle of Power Screw given Load and Coefficient of Friction

$$lpha = a aniggl(rac{\mathrm{W} \cdot \mu \cdot \mathrm{sec}(0.253) - \mathrm{P_{lo}}}{\mathrm{W} + (\mathrm{P_{lo}} \cdot \mu \cdot \mathrm{sec}(0.253))} iggr)$$

$$\mathbf{x} \left(4.769225^{\circ} = a \tan \left(\frac{1700 \mathrm{N} \cdot 0.15 \cdot \mathrm{sec}(0.253) - 120 \mathrm{N}}{1700 \mathrm{N} + (120 \mathrm{N} \cdot 0.15 \cdot \mathrm{sec}(0.253))} \right) \right)$$

10) Helix Angle of Power Screw given Torque Required in Lifting Load with Acme Threaded Screw

$$\int \alpha = a \tan \left(\frac{2 \cdot \mathrm{Mt}_{\mathrm{li}} - \mathrm{W} \cdot \mathrm{d}_{\mathrm{m}} \cdot \mu \cdot \mathrm{sec}\left(0.253 \cdot \frac{\pi}{180}\right)}{\mathrm{W} \cdot \mathrm{d}_{\mathrm{m}} + 2 \cdot \mathrm{Mt}_{\mathrm{li}} \cdot \mu \cdot \mathrm{sec}\left(0.253 \cdot \frac{\pi}{180}\right)} \right)$$
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$$4.799891^{\circ} = a \tan \left(\frac{2 \cdot 9265 \text{N*mm} - 1700 \text{N} \cdot 46 \text{mm} \cdot 0.15 \cdot \sec \left(0.253 \cdot \frac{\pi}{180} \right)}{1700 \text{N} \cdot 46 \text{mm} + 2 \cdot 9265 \text{N*mm} \cdot 0.15 \cdot \sec \left(0.253 \cdot \frac{\pi}{180} \right)} \right)$$





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11) Helix Angle of Power Screw given Torque Required in Lowering Load with Acme Threaded Screw

fx
$$lpha = a aniggl(rac{\mathrm{W} \cdot \mathrm{d_m} \cdot \mu \cdot \mathrm{sec}(0.253) - 2 \cdot \mathrm{Mt_{lo}}}{\mathrm{W} \cdot \mathrm{d_m} + 2 \cdot \mathrm{Mt_{lo}} \cdot \mu \cdot \mathrm{sec}(0.253)} iggr)$$

$$\mathbf{ex} \left[4.477712^{\circ} = a \tan \left(\frac{1700 \mathrm{N} \cdot 46 \mathrm{mm} \cdot 0.15 \cdot \mathrm{sec}(0.253) - 2 \cdot 2960 \mathrm{N}^* \mathrm{mm}}{1700 \mathrm{N} \cdot 46 \mathrm{mm} + 2 \cdot 2960 \mathrm{N}^* \mathrm{mm} \cdot 0.15 \cdot \mathrm{sec}(0.253)} \right) \right)$$

12) Load on Power Screw given Effort Required in Lifting Load with Acme Threaded Screw

fx
$$\mathbf{W} = \mathbf{P}_{\mathrm{li}} \cdot rac{1 - \mu \cdot \mathrm{sec}((0.253)) \cdot \mathrm{tan}(\alpha)}{\mu \cdot \mathrm{sec}((0.253)) + \mathrm{tan}(\alpha)}$$

$$1699.661 \text{N} = 402 \text{N} \cdot \frac{1 - 0.15 \cdot \sec((0.253)) \cdot \tan(4.5^{\circ})}{0.15 \cdot \sec((0.253)) + \tan(4.5^{\circ})}$$

13) Load on Power Screw given Effort Required in Lowering Load with Acme Threaded Screw

$$\mathbf{\vec{x}} = P_{lo} \cdot \frac{1 + \mu \cdot \sec((0.253)) \cdot \tan(\alpha)}{\mu \cdot \sec((0.253)) - \tan(\alpha)}$$

$$\textbf{ex} \ 1593.369 \text{N} = 120 \text{N} \cdot \frac{1 + 0.15 \cdot \sec((0.253)) \cdot \tan(4.5^\circ)}{0.15 \cdot \sec((0.253)) - \tan(4.5^\circ)}$$

14) Load on Power Screw given Torque Required in Lifting Load with Acme Threaded Screw



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Open Calculator 🕑

15) Load on Power Screw given Torque Required in Lowering Load with Acme Threaded Screw

$$\begin{aligned} & \textbf{fx} \end{bmatrix} W = 2 \cdot M t_{lo} \cdot \frac{1 + \mu \cdot \sec((0.253)) \cdot \tan(\alpha)}{d_m \cdot (\mu \cdot \sec((0.253)) - \tan(\alpha))} \end{aligned}$$

$$1708.831 \text{N} = 2 \cdot 2960 \text{N*mm} \cdot \frac{1 + 0.15 \cdot \sec((0.253)) \cdot \tan(4.5^{\circ})}{46 \text{mm} \cdot (0.15 \cdot \sec((0.253)) - \tan(4.5^{\circ}))}$$

16) Mean Diameter of Power Screw given Torque Required in Lowering Load with Acme Threaded Screw

fx
$$d_{\mathrm{m}} = 2 \cdot \mathrm{Mt}_{\mathrm{lo}} \cdot rac{1 + \mu \cdot \mathrm{sec}((0.253)) \cdot \mathrm{tan}(\alpha)}{\mathrm{W} \cdot (\mu \cdot \mathrm{sec}((0.253)) - \mathrm{tan}(\alpha))}$$

$$\textbf{ex} \ 46.23895 \text{mm} = 2 \cdot 2960 \text{N*mm} \cdot \frac{1 + 0.15 \cdot \text{sec}((0.253)) \cdot \tan(4.5\degree)}{1700 \text{N} \cdot (0.15 \cdot \text{sec}((0.253)) - \tan(4.5\degree))}$$

17) Torque Required in Lifting Load with Acme Threaded Power Screw 🕑

$$\begin{aligned} & \overbrace{\mathbf{Mt}_{li} = 0.5 \cdot d_m \cdot W \cdot \left(\frac{\mu \cdot \sec((0.253)) + \tan(\alpha)}{1 - \mu \cdot \sec((0.253)) \cdot \tan(\alpha)}\right)} \\ & \underbrace{\mathbf{Mt}_{li} = 0.5 \cdot d_m \cdot W \cdot \left(\frac{\mu \cdot \sec((0.253)) \cdot \tan(\alpha)}{1 - \mu \cdot \sec((0.253)) \cdot \tan(4.5^\circ)}\right)} \\ & \underbrace{\mathbf{P}_{247.846N*mm} = 0.5 \cdot 46 \text{mm} \cdot 1700 \text{N} \cdot \left(\frac{0.15 \cdot \sec((0.253)) + \tan(4.5^\circ)}{1 - 0.15 \cdot \sec((0.253)) \cdot \tan(4.5^\circ)}\right)} \end{aligned}$$

)

Open Calculator



fx

ex

18) Torque Required in Lowering Load with Acme Threaded Power Screw 🕑

$$\mathrm{Mt}_{\mathrm{lo}} = 0.5 \cdot \mathrm{d}_{\mathrm{m}} \cdot \mathrm{W} \cdot \left(rac{(\mu \cdot \mathrm{sec}((0.253))) - \mathrm{tan}(lpha)}{1 + (\mu \cdot \mathrm{sec}((0.253)) \cdot \mathrm{tan}(lpha))}
ight)$$

 $2944.704\text{N*mm} = 0.5 \cdot 46\text{mm} \cdot 1700\text{N} \cdot \left(\frac{(0.15 \cdot \sec((0.253))) - \tan(4.5^{\circ})}{1 + (0.15 \cdot \sec((0.253)) \cdot \tan(4.5^{\circ}))}\right)$

Torque Requirement in Lowering Load using Square threaded Screws

fx
$$\mu = rac{\mathrm{P_{lo}} + \mathrm{tan}(lpha) \cdot \mathrm{W}}{\mathrm{W} - \mathrm{P_{lo}} \cdot \mathrm{tan}(lpha)}$$

$$\mathbf{x} 0.150124 = \frac{120\mathrm{N} + \mathrm{tan}(4.5^{\circ}) \cdot 1700\mathrm{N}}{1700\mathrm{N} - 120\mathrm{N} \cdot \mathrm{tan}(4.5^{\circ})}$$

20) Coefficient of Friction of Screw Thread given Torque Required in Lowering Load

$$\mathbf{x} \left[\mu = rac{2 \cdot \mathrm{Mt_{lo}} + \mathrm{W} \cdot \mathrm{d_m} \cdot \mathrm{tan}(lpha)}{\mathrm{W} \cdot \mathrm{d_m} - 2 \cdot \mathrm{Mt_{lo}} \cdot \mathrm{tan}(lpha)}
ight]$$



Open Calculator 🖒

21) Effort Required in Lowering Load C

fx
$$\mathbf{P}_{\mathrm{lo}} = \mathrm{W} \cdot \left(rac{\mu - \mathrm{tan}(lpha)}{1 + \mu \cdot \mathrm{tan}(lpha)}
ight)$$

$$119.7929 \mathrm{N} = 1700 \mathrm{N} \cdot \left(\frac{0.15 - \tan(4.5^{\circ})}{1 + 0.15 \cdot \tan(4.5^{\circ})}\right)$$

22) Helix Angle of Power Screw given Effort Required in Lowering Load 🕻

fx
$$lpha = a an igg(rac{\mathrm{W} \cdot \mu - \mathrm{P_{lo}}}{\mu \cdot \mathrm{P_{lo}} + \mathrm{W}} igg)$$

$$4.493055^{\circ} = a \tan\left(\frac{1700\text{N} \cdot 0.15 - 120\text{N}}{0.15 \cdot 120\text{N} + 1700\text{N}}\right)$$

23) Helix Angle of Power Screw given Torque Required in Lowering Load 🗹

Open Calculator 🕑

Open Calculator

$$lpha = a an iggl(rac{\mu \cdot \mathrm{W} \cdot \mathrm{d_m} - (2 \cdot \mathrm{Mt_{lo}})}{2 \cdot \mathrm{Mt_{lo}} \cdot \mu + (\mathrm{W} \cdot \mathrm{d_m})} iggr)$$

 $\overbrace{\text{ex}}{4.201542^{\circ} = a \tan \left(\frac{0.15 \cdot 1700\text{N} \cdot 46\text{mm} - (2 \cdot 2960\text{N}^*\text{mm})}{2 \cdot 2960\text{N}^*\text{mm} \cdot 0.15 + (1700\text{N} \cdot 46\text{mm})} \right)}$

24) Load on power Screw given Effort Required in Lowering Load 🕻

$$\mathbf{fx} \mathbf{W} = \frac{\mathbf{P}_{lo}}{\frac{\mu - \tan(\alpha)}{1 + \mu \cdot \tan(\alpha)}}$$

$$\mathbf{ex} \mathbf{1702.939N} = \frac{\mathbf{120N}}{\frac{0.15 - \tan(4.5^{\circ})}{1 + 0.15 \cdot \tan(4.5^{\circ})}}$$



Open Calculator



25) Load on power Screw given Torque Required in Lowering Load 🕑

$$\begin{aligned} & \textbf{fx} \mathbf{W} = \frac{\mathrm{Mt}_{\mathrm{lo}}}{0.5 \cdot \mathrm{d_m} \cdot \left(\frac{\mu - \tan(\alpha)}{1 + \mu \cdot \tan(\alpha)}\right)} \\ & \textbf{ex} \mathbf{1826.34N} = \frac{2960 \mathrm{N}^* \mathrm{mm}}{0.5 \cdot 46 \mathrm{mm} \cdot \left(\frac{0.15 - \tan(4.5^\circ)}{1 + 0.15 \cdot \tan(4.5^\circ)}\right)} \end{aligned}$$

26) Mean Diameter of Power Screw given Torque Required in Lowering Load

Open Calculator 🕑

Open Calculator 🕑

Open Calculator

fx
$$d_{\mathrm{m}} = rac{\mathrm{Mt}_{\mathrm{lo}}}{0.5 \cdot \mathrm{W} \cdot \left(rac{\mu - \mathrm{tan}(lpha)}{1 + \mu \cdot \mathrm{tan}(lpha)}
ight)}$$

27) Torque Required in Lowering Load on Power Screw 🕑

fx
$$Mt_{lo} = 0.5 \cdot W \cdot d_m \cdot \left(rac{\mu - an(lpha)}{1 + \mu \cdot an(lpha)}
ight)$$

ex
$$2755.237 \text{N*mm} = 0.5 \cdot 1700 \text{N} \cdot 46 \text{mm} \cdot \left(\frac{0.15 - \tan(4.5^{\circ})}{1 + 0.15 \cdot \tan(4.5^{\circ})}\right)$$

Collar Friction





31) Collar Friction Torque for Screw according to Uniform Wear Theory

$$\label{eq:collar} \begin{split} & \textbf{K} \ \mathbf{T}_c = \mu_{collar} \cdot \mathbf{W} \cdot \frac{\mathbf{R}_1 + \mathbf{R}_2}{2} \\ \\ & \textbf{ex} \ 11696 N^* mm = 0.16 \cdot 1700 N \cdot \frac{54 mm + 32 mm}{2} \end{split}$$

32) Load on Screw given Collar Friction Torque according to Uniform Pressure Theory

$$\mathbb{E} \mathbf{W} = \frac{3 \cdot \mathbf{T}_{c} \cdot \left(\left(\mathbf{D}_{o}^{2} \right) - \left(\mathbf{D}_{i}^{2} \right) \right)}{\mu_{collar} \cdot \left(\left(\mathbf{D}_{o}^{3} \right) - \left(\mathbf{D}_{i}^{3} \right) \right)}$$

$$\mathbb{E} \mathbf{W} = \frac{3 \cdot 10000 \mathrm{N*mm} \cdot \left(\left((100 \mathrm{mm})^{2} \right) - \left((60 \mathrm{mm})^{2} \right) \right)}{0.16 \cdot \left(\left((100 \mathrm{mm})^{3} \right) - \left((60 \mathrm{mm})^{3} \right) \right)}$$

$$\begin{aligned} &\mathsf{fx} \mathbf{W} = \frac{4 \cdot \mathbf{T}_{c}}{\mu_{collar} \cdot ((\mathbf{D}_{o}) + (\mathbf{D}_{i}))} \end{aligned}$$

$$&\mathsf{ex} 1562.5\mathrm{N} = \frac{4 \cdot 10000\mathrm{N*mm}}{0.16 \cdot ((100\mathrm{mm}) + (60\mathrm{mm}))} \end{aligned}$$



Design of Screw and Nut 🕑

34) Axial Load on Screw given Direct Compressive Stress 🕑

$$\mathbf{W}_{a} = \frac{\sigma_{c} \cdot \pi \cdot d_{c}^{2}}{4}$$

$$\mathbf{W}_{a} = \frac{\sigma_{c} \cdot \pi \cdot d_{c}^{2}}{4}$$

$$\mathbf{W}_{a} = \frac{94N/\text{mm}^{2} \cdot \pi \cdot (42\text{mm})^{2}}{4}$$

$$\mathbf{S}_{a} = \frac{94N/\text{mm}^{2} \cdot \pi \cdot (42\text{mm})^{2}}{4}$$

$$\mathbf{S}_{a} = \frac{94N/\text{mm}^{2} \cdot \pi \cdot (42\text{mm})^{2}}{4}$$

$$\mathbf{S}_{a} = \frac{1}{(\tau_{s} \cdot \pi \cdot d_{c} \cdot t \cdot z)}$$

$$\mathbf{O}_{pen} \text{ Calculator } \mathbf{S}_{a}$$

$$\mathbf{S}_{a} = \frac{1}{(\tau_{s} \cdot \pi \cdot d_{c} \cdot t \cdot z)}$$

$$\mathbf{O}_{pen} \text{ Calculator } \mathbf{S}_{a}$$

$$\mathbf{S}_{a} = \frac{1}{(\tau_{s} \cdot \pi \cdot d_{c} \cdot t \cdot z)}$$

$$\mathbf{O}_{pen} \text{ Calculator } \mathbf{S}_{a}$$

$$\mathbf{S}_{a} = \frac{1}{(\tau_{s} \cdot \pi \cdot t \cdot d_{c} \cdot t \cdot z)}$$

$$\mathbf{O}_{pen} \text{ Calculator } \mathbf{S}_{a}$$

$$\mathbf{S}_{a} = \frac{1}{(\tau_{s} \cdot \pi \cdot t \cdot d \cdot z)}$$

$$\mathbf{O}_{pen} \text{ Calculator } \mathbf{S}_{a}$$

$$\mathbf{S}_{a} = \frac{\pi \cdot t_{n} \cdot t \cdot d \cdot z}$$

$$\mathbf{O}_{pen} \text{ Calculator } \mathbf{S}_{a}$$

$$\mathbf{S}_{a} = \frac{\pi \cdot z \cdot S_{b} \cdot \frac{(d^{2}) - (d_{c}^{2})}{4}}$$

$$\mathbf{S}_{a} = \frac{\pi \cdot z \cdot S_{b} \cdot \frac{(d^{2}) - (d_{c}^{2})}{4}}$$

$$\mathbf{S}_{a} = \frac{129541.7N}{4} = \pi \cdot 9 \cdot 24.9N/\text{mm}^{2} \cdot \frac{((50\text{mm})^{2}) - ((42\text{mm})^{2})}{4}$$



38) Bearing Area between Screw and Nut for One Thread 🕑





42) Core Diameter of Screw given Transverse Shear Stress in Screw 🕑

$$d_{c} = \frac{W_{a}}{\tau_{s} \cdot \pi \cdot t \cdot z}$$

$$d_{c} = \frac{W_{a}}{\tau_{s} \cdot \pi \cdot t \cdot z}$$

$$(2) 41.96719mm = \frac{131000N}{27.6N/mm^{2} \cdot \pi \cdot 4mm \cdot 9}$$

$$(3) \text{ Core Diameter of Screw given Unit Bearing Pressure }$$

$$(4) \text{ Core Diameter of Screw given Unit Bearing Pressure }$$

$$(5) d_{c} = \sqrt{(d)^{2} - \left(4 \cdot \frac{W_{a}}{S_{b} \cdot \pi \cdot z}\right)}$$

$$(4) \text{ Direct Compressive Stress in Screw }$$

$$(4) \text{ Direct Compressive Stress in Screw }$$

$$(5) \text{ Weight and a stress of the stress in Screw }$$

$$(5) \text{ Pen Calculator }$$

$$(6) \text{ Pen Calculator }$$

$$(7) \text{ Pen Calculator }$$

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$$(7) \text{ Pen Calculator }$$

$$(8) \text{ Pen Calculator }$$

$$(8) \text{ Pen Calculator }$$

$$(8) \text{ Pen Calculator }$$

$$(9) \text{ Pen Calculator$$





46) Lead of Screw given Helix angle Open Calculator fx $L = tan(\alpha) \cdot \pi \cdot d_m$ ex 11.37344mm = tan $(4.5^{\circ}) \cdot \pi \cdot 46$ mm 47) Lead of Screw given Overall Efficiency Open Calculator $\mathbf{K} \ \mathrm{L} = 2 \cdot \pi \cdot \eta \cdot rac{\mathrm{Mt_t}}{\mathrm{W_a}}$ ex 11.05769mm = $2 \cdot \pi \cdot 0.35 \cdot \frac{658700$ N*mm}{131000N} 48) Mean Diameter of Power Screw Open Calculator fx $m d_m =
m d - 0.5 \cdot
m p$ ex 46.1mm = 50mm - $0.5 \cdot 7.8$ mm 49) Mean diameter of Screw given Helix Angle 🗹 Open Calculator $\mathbf{f} \mathbf{x} d_{\mathrm{m}} = rac{\mathrm{L}}{\pi \cdot \mathrm{tan}(\alpha)}$ $ex 44.48962 \text{mm} = \frac{11 \text{mm}}{\pi \cdot \tan(4.5^\circ)}$ 50) Nominal Diameter of Power Screw 🖸 Open Calculator fx $d = d_c + p$

$$\begin{array}{c} \textbf{ex} \hspace{0.1cm} 49.8 \text{mm} = 42 \text{mm} + 7.8 \text{mm} \end{array}$$

15/35

51) Nominal Diameter of Power Screw given Mean Diameter 🕑

$$\mathbf{k} \ \mathbf{d} = \mathbf{d}_{m} + (0.5 \cdot \mathbf{p})$$
Open Calculator C
$$\mathbf{k} \ 49.9 \text{mm} = 46 \text{mm} + (0.5 \cdot 7.8 \text{mm})$$
52) Nominal Diameter of Screw given Transverse Shear Stress at Root of Nut C
$$\mathbf{k} \ \mathbf{d} = \frac{W_{a}}{\pi \cdot \mathbf{t}_{n} \cdot \mathbf{t} \cdot z}$$
Open Calculator C
$$\mathbf{k} \ \mathbf{d} = \frac{W_{a}}{\pi \cdot \mathbf{t}_{n} \cdot \mathbf{t} \cdot z}$$
53) Nominal Diameter of Screw given Unit Bearing Pressure C
$$\mathbf{k} \ \mathbf{d} = \sqrt{\left(4 \cdot \frac{W_{a}}{S_{b} \cdot \pi \cdot z}\right) + (d_{c})^{2}}$$
Open Calculator C
$$\mathbf{k} \ \mathbf{d} = \sqrt{\left(4 \cdot \frac{131000\text{N}}{24.9\text{N/mm}^{2} \cdot \pi \cdot 9}\right) + (42\text{mm})^{2}}$$
54) Number of Threads in Engagement with Nut given Transverse Shear Stress C
$$\mathbf{k} \ \mathbf{z} = \frac{W_{a}}{\pi \cdot \mathbf{t} \cdot \mathbf{\tau}_{s} \cdot \mathbf{d}_{c}}$$
Open Calculator C
$$\mathbf{k} \ \mathbf{d} = \sqrt{\frac{W_{a}}{\pi \cdot \mathbf{t} \cdot \mathbf{t}_{s} \cdot \mathbf{d}_{c}}}$$

ex
$$8.992968 = rac{131000 \mathrm{N}}{\pi \cdot 4 \mathrm{mm} \cdot 27.6 \mathrm{N/mm^2} \cdot 42 \mathrm{mm}}$$

55) Number of Threads in Engagement with Nut given Transverse Shear Stress at Root of Nut

Open Calculator 🕑



56) Number of Threads in Engagement with Nut given Unit Bearing Pressure 🕑

$$fx = 4 \cdot \frac{W_a}{(\pi \cdot S_b \cdot ((d^2) - (d_c^2)))}$$

$$fx = 4 \cdot \frac{W_a}{(\pi \cdot S_b \cdot ((d^2) - (d_c^2)))}$$

$$fx = 9.101317 = 4 \cdot \frac{131000N}{(\pi \cdot 24.9N/mm^2 \cdot (((50mm)^2) - ((42mm)^2)))}$$

$$fy = W_a \cdot \frac{L}{2 \cdot \pi \cdot Mt_t}$$

$$fx = W_a \cdot \frac{L}{2 \cdot \pi \cdot Mt_t}$$

$$fx = 0.348174 = 131000N \cdot \frac{11mm}{2 \cdot \pi \cdot 658700N^*mm}$$

$$fx = d - d_c$$

$$fx = d - d_c$$

$$fx = 50mm - 42mm$$

$$fx = 50mm - 42mm$$



Open Calculator

Open Calculator

59) Pitch of Screw given Mean Diameter 🕑





61) Thread Thickness at Root of Nut given Transverse Shear Stress at Root of Nut

fx
$$\mathbf{t} = rac{\mathbf{W_a}}{\pi \cdot \mathbf{d} \cdot \mathbf{z} \cdot \mathbf{t_n}}$$

ex
$$3.976976 \mathrm{mm} = rac{131000 \mathrm{N}}{\pi \cdot 50 \mathrm{mm} \cdot 9 \cdot 23.3 \mathrm{N/mm^2}}$$

62) Torsional Moment in Screw given Torsional Shear Stress 🖸

$$fx Mt_t = \tau \cdot \pi \cdot \frac{d_c^3}{16}$$

$$ex 658694.7N^*mm = 45.28N/mm^2 \cdot \pi \cdot \frac{(42mm)^3}{16}$$

16





63) Torsional Shear Stress of Screw 🕑

$$\mathbf{f} = 16 \cdot \frac{Mt_{t}}{\pi \cdot (d_{c}^{3})}$$

$$\mathbf{f} = 16 \cdot \frac{Mt_{t}}{\pi \cdot (d_{c}^{3})}$$

$$\mathbf{f} = 16 \cdot \frac{658700N^{*}mm}{\pi \cdot ((42mm)^{3})}$$

$$\mathbf{f} = \frac{45.28036N/mm^{2}}{\pi \cdot d_{c} t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} \cdot t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} \cdot t \cdot z}$$

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$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} \cdot t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} \cdot t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} \cdot t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} \cdot t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} \cdot t \cdot z}$$

$$\mathbf{f} = \frac{W_{a}}{\pi \cdot d_{c} \cdot t \cdot z}$$

$$\mathbf{f} = \frac{131000N}{\pi \cdot 42mm \cdot 4mm \cdot 9}$$

$$\mathbf{f} = \frac{131000N}{\pi \cdot 2 \cdot ((d^{2}) - (d_{c}^{2}))}$$

$$\mathbf{f} = \frac{25.18031N/mm^{2}}{\pi \cdot 9 \cdot (((50mm)^{2}) - ((42mm)^{2}))}$$



Torque Requirement in Lifting Load using Square Threaded Screw

67) Coefficient of Friction for Screw Thread given Efficiency of Square Threaded Screw

$$\mu = rac{ an(lpha) \cdot (1-\eta)}{ an(lpha) \cdot an(lpha) + \eta}$$

 $fx \mu = \frac{P_{li} - W \cdot tan(\alpha)}{W + P_{li} - tan(\alpha)}$

ex
$$0.143619 = \frac{\tan(4.5\degree) \cdot (1 - 0.35)}{\tan(4.5\degree) \cdot \tan(4.5\degree) + 0.35}$$

68) Coefficient of Friction of Power Screw given Effort Required to Lift Load 🕑

Open Calculator 🕑

Open Calculator

$$\mathbf{ex} 0.154886 = \frac{402N - 1700N \cdot \tan(4.5^{\circ})}{1700N + 402N \cdot \tan(4.5^{\circ})}$$

69) Coefficient of Friction of Power Screw given Torque Required to Lift Load 🕑

fx
$$\mu = rac{\left(2 \cdot rac{\mathrm{Mt}_{\mathrm{li}}}{\mathrm{d}_{\mathrm{m}}}
ight) - \mathrm{W} \cdot \mathrm{tan}(lpha)}{\mathrm{W} - \left(2 \cdot rac{\mathrm{Mt}_{\mathrm{li}}}{\mathrm{d}_{\mathrm{m}}}
ight) \cdot \mathrm{tan}(lpha)}$$

$$ex 0.161262 = \frac{\left(2 \cdot \frac{9265\text{N}^*\text{mm}}{46\text{mm}}\right) - 1700\text{N} \cdot \tan(4.5^\circ)}{1700\text{N} - \left(2 \cdot \frac{9265\text{N}^*\text{mm}}{46\text{mm}}\right) \cdot \tan(4.5^\circ)}$$



70) Efficiency of Square Threaded Power Screw 🕑

$$f_{\mathbf{X}} \eta = \frac{\tan(\alpha)}{\frac{\mu + \tan(\alpha)}{1 - \mu \cdot \tan(\alpha)}}$$

$$e_{\mathbf{X}} 0.340061 = \frac{\tan(4.5^{\circ})}{\frac{0.15 + \tan(4.5^{\circ})}{1 - 0.15 \cdot \tan(4.5^{\circ})}}$$

$$71) \text{ Effort Required in Lifting load using Power Screw } \checkmark$$

fx
$$\mathbf{P}_{\mathrm{li}} = \mathrm{W} \cdot \left(rac{\mu + \mathrm{tan}(lpha)}{1 - \mu \cdot \mathrm{tan}(lpha)}
ight)$$

$$\begin{array}{c} \textbf{x} \end{array} 393.4375 \text{N} = 1700 \text{N} \cdot \left(\frac{0.15 + \tan(4.5°)}{1 - 0.15 \cdot \tan(4.5°)} \right) \end{array}$$

72) Effort Required to Lift Load given Torque Required to Lift Load C

fx
$$P_{li} = 2 \cdot rac{M t_{li}}{d_m}$$
 (Open Calculator (2)

ex
$$402.8261$$
N $= 2 \cdot \frac{9265$ N*mm}{46mm

73) External Torque required to raise Load given Efficiency

$$f_{\mathbf{X}} M t_{t} = W_{a} \cdot \frac{L}{2 \cdot \pi \cdot \eta}$$

$$e_{\mathbf{X}} 655263.6N^{*}mm = 131000N \cdot \frac{11mm}{2 \cdot \pi \cdot 0.35}$$
Open Calculator



74) Helix Angle of Power Screw given Effort Required to Lift Load 🖸

$$\begin{aligned} & \mathbf{fx} \ \alpha = a \tan \left(\frac{\mathbf{P}_{\mathrm{li}} - \mathbf{W} \cdot \mathbf{\mu}}{\mathbf{P}_{\mathrm{li}} \cdot \mathbf{\mu} + \mathbf{W}} \right) \end{aligned} \tag{Open Calculator } \\ & \mathbf{ex} \ 4.773608^{\circ} = a \tan \left(\frac{402\mathrm{N} - 1700\mathrm{N} \cdot 0.15}{402\mathrm{N} \cdot 0.15 + 1700\mathrm{N}} \right) \end{aligned}$$

75) Helix Angle of Power Screw given Torque Required to Lift Load 🕑

$$lpha = a an igg(rac{2 \cdot \mathrm{Mt_{li}} - \mathrm{W} \cdot \mathrm{d_m} \cdot \mu}{2 \cdot \mathrm{Mt_{li}} \cdot \mu + \mathrm{W} \cdot \mathrm{d_m}} igg)$$

 $\underbrace{\mathsf{ex}} 4.799973^{\circ} = a \tan \left(\frac{2 \cdot 9265 \mathrm{N*mm} - 1700 \mathrm{N} \cdot 46 \mathrm{mm} \cdot 0.15}{2 \cdot 9265 \mathrm{N*mm} \cdot 0.15 + 1700 \mathrm{N} \cdot 46 \mathrm{mm}} \right)$

76) Load on Power Screw given Effort Required to Lift Load 🕑

$$fx W = \frac{P_{li}}{\frac{\mu + \tan(\alpha)}{1 - \mu \cdot \tan(\alpha)}}$$

$$ex 1736.997N = \frac{402N}{\frac{0.15 + \tan(4.5^{\circ})}{1 - 0.15 \cdot \tan(4.5^{\circ})}}$$

77) Load on Power Screw given Torque Required to Lift Load 🕑

$$\mathbf{fx} \mathbf{W} = \left(2 \cdot \frac{\mathrm{Mt_{li}}}{\mathrm{d_m}}\right) \cdot \left(\frac{1 - \mu \cdot \tan(\alpha)}{\mu + \tan(\alpha)}\right)$$
$$\mathbf{ex} \mathbf{1740.567N} = \left(2 \cdot \frac{9265\mathrm{N*mm}}{46\mathrm{mm}}\right) \cdot \left(\frac{1 - 0.15 \cdot \tan(4.5^\circ)}{0.15 + \tan(4.5^\circ)}\right)$$



Open Calculator

78) Load on Screw given Overall Efficiency Open Calculator fx $\mathrm{W_a} = 2 \cdot \pi \cdot \mathrm{Mt_t} \cdot rac{\eta}{\mathrm{L}}$ ex 131687N = $2 \cdot \pi \cdot 658700$ N*mm $\cdot \frac{0.35}{11$ mm 79) Maximum Efficiency of Square Threaded Screw 🖒 Open Calculator $\eta_{\max} = rac{1 - \sin(a \tan(\mu))}{1 + \sin(a \tan(\mu))}$ ex $0.741644 = \frac{1 - \sin(a \tan(0.15))}{1 + \sin(a \tan(0.15))}$ 80) Mean Diameter of Power Screw given Torque Required to Lift Load 🕑 Open Calculator fx $ext{d}_{ ext{m}} = 2 \cdot rac{ ext{Mt}_{ ext{li}}}{ ext{Pu}}$ ex 46.09453mm $= 2 \cdot \frac{9265$ N*mm}{402N} 81) Torque Required to Lift Load given Effort 🕑 Open Calculator fx $Mt_{li} = P_{li} \cdot \frac{d_m}{2}$

$$ex 9246 \text{N*mm} = 402 \text{N} \cdot \frac{46 \text{mm}}{2}$$



82) Torque Required to Lift Load given Load 🕑

fx
$$Mt_{li} = \left(W \cdot \frac{d_m}{2}\right) \cdot \left(\frac{\mu + \tan(\alpha)}{1 - \mu \cdot \tan(\alpha)}\right)$$

$$\begin{array}{c} \texttt{ex} \end{array} 9049.063 \text{N*mm} = \left(1700 \text{N} \cdot \frac{46 \text{mm}}{2} \right) \cdot \left(\frac{0.15 + \tan(4.5°)}{1 - 0.15 \cdot \tan(4.5°)} \right) \end{array}$$

Trapezoidal Thread 🕑

83) Coefficient of Friction of Power Screw given Efficiency of Trapezoidal Threaded Screw

fx
$$\mu = (\tan(\alpha)) \cdot rac{1 - \eta}{\sec(0.253) \cdot \left(\eta + (\tan(\alpha))^2\right)}$$

$$\textbf{ex} 0.139047 = (\tan(4.5\degree)) \cdot \frac{1 - 0.35}{\sec(0.253) \cdot \left(0.35 + (\tan(4.5\degree))^2\right)}$$

84) Coefficient of Friction of Screw given Efficiency of Trapezoidal Threaded Screw

$$f_{\mathbf{X}} \mu = \tan(\alpha) \cdot \frac{1 - \eta}{\sec(0.2618) \cdot (\eta + \tan(\alpha) \cdot \tan(\alpha))}$$

$$e_{\mathbf{X}} 0.138725 = \tan(4.5^{\circ}) \cdot \frac{1 - 0.35}{\sec(0.2618) \cdot (0.35 + \tan(4.5^{\circ}) \cdot \tan(4.5^{\circ}))}$$

Open Calculator

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85) Coefficient of Friction of Screw given Effort for Trapezoidal Threaded Screw 🕑

$$\mu = rac{\mathrm{P}_{\mathrm{li}} - (\mathrm{W} \cdot \mathrm{tan}(lpha))}{\mathrm{sec}(0.2618) \cdot (\mathrm{W} + \mathrm{P}_{\mathrm{li}} \cdot \mathrm{tan}(lpha))}$$

$$\textbf{ex} 0.149609 = \frac{402 \text{N} - (1700 \text{N} \cdot \tan(4.5^{\circ}))}{\sec(0.2618) \cdot (1700 \text{N} + 402 \text{N} \cdot \tan(4.5^{\circ}))}$$

86) Coefficient of Friction of Screw given Effort in Lowering Load 🕑

$$=rac{\mathrm{P}_{\mathrm{lo}}+\mathrm{W}\cdot\mathrm{tan}(lpha)}{\mathrm{W}\cdot\mathrm{sec}(0.2618)-\mathrm{P}_{\mathrm{lo}}\cdot\mathrm{sec}(0.2618)\cdot\mathrm{tan}(lpha)}$$

$$\textbf{ex} \ 0.145009 = \frac{120 \text{N} + 1700 \text{N} \cdot \tan(4.5\degree)}{1700 \text{N} \cdot \sec(0.2618) - 120 \text{N} \cdot \sec(0.2618) \cdot \tan(4.5\degree)}$$

87) Coefficient of Friction of Screw given Torque Required in Lifting Load with Trapezoidal Thread

$$f_{\mathbf{X}} \mu = \frac{2 \cdot Mt_{li} - W \cdot d_{m} \cdot tan(\alpha)}{\sec(0.2618) \cdot (W \cdot d_{m} + 2 \cdot Mt_{li} \cdot tan(\alpha))}$$

$$e_{\mathbf{X}} 0.150064 = \frac{2 \cdot 9265N^{*}mm - 1700N \cdot 46mm \cdot tan(4.5^{\circ})}{\sec(0.2618) \cdot (1700N \cdot 46mm + 2 \cdot 9265N^{*}mm \cdot tan(4.5^{\circ}))}$$

88) Coefficient of Friction of Screw given Torque Required in Lowering Load with Trapezoidal Thread

$$\mathbf{fx} \mu = \frac{2 \cdot Mt_{lo} + W \cdot d_m \cdot tan(\alpha)}{\sec(0.2618) \cdot (W \cdot d_m - 2 \cdot Mt_{lo} \cdot tan(\alpha))}$$

$$\mathbf{fx} 0.150038 = \frac{2 \cdot 2960N^*mm + 1700N \cdot 46mm \cdot tan(4.5^{\circ})}{\sec(0.2618) \cdot (1700N \cdot 46mm - 2 \cdot 2960N^*mm \cdot tan(4.5^{\circ}))}$$





Open Calculator

Open Calculator

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89) Efficiency of Trapezoidal Threaded Screw 🕑

$$\int \mathbf{x} \eta = an(lpha) \cdot rac{1 - \mu \cdot an(lpha) \cdot \sec(0.2618)}{\mu \cdot \sec(0.2618) + an(lpha)}$$

$$0.332231 = \tan(4.5^{\circ}) \cdot \frac{1 - 0.15 \cdot \tan(4.5^{\circ}) \cdot \sec(0.2618)}{0.15 \cdot \sec(0.2618) + \tan(4.5^{\circ})}$$

90) Effort Required in Lifting Load with Trapezoidal Threaded Screw 🕑

Open Calculator 🗹

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$$\left| \mathbf{P}_{li} = \mathbf{W} \cdot \left(\frac{\mu \cdot \sec((0.2618)) + \tan(\alpha)}{1 - \mu \cdot \sec((0.2618)) \cdot \tan(\alpha)} \right) \right|$$

 $\mathbf{ex} \ 402.7102 \mathrm{N} = 1700 \mathrm{N} \cdot \left(\frac{0.15 \cdot \mathrm{sec}((0.2618)) + \mathrm{tan}(4.5\degree)}{1 - 0.15 \cdot \mathrm{sec}((0.2618)) \cdot \mathrm{tan}(4.5\degree)} \right)$

91) Effort Required in Lowering Load with Trapezoidal Threaded Screw 🕑

$$\mathbf{P}_{\mathrm{lo}} = \mathrm{W} \cdot \left(\frac{\mu \cdot \sec((0.2618)) - \tan(\alpha)}{1 + \mu \cdot \sec((0.2618)) \cdot \tan(\alpha)} \right)$$

 $lpha = a aniggl(rac{ ext{P}_{ ext{li}} - ext{W} \cdot \mu \cdot ext{sec}(0.2618)}{ ext{W} + (ext{P}_{ ext{li}} \cdot \mu \cdot ext{sec}(0.2618))} iggr)$

$$\underbrace{128.6305\mathrm{N} = 1700\mathrm{N} \cdot \left(\frac{0.15 \cdot \mathrm{sec}((0.2618)) - \mathrm{tan}(4.5\degree)}{1 + 0.15 \cdot \mathrm{sec}((0.2618)) \cdot \mathrm{tan}(4.5\degree)}\right) }$$

 $ex 4.477334^{\circ} = a \tan\left(\frac{402N - 1700N \cdot 0.15 \cdot \sec(0.2618)}{1700N + (402N \cdot 0.15 \cdot \sec(0.2618))}\right)$

92) Helix Angle of Screw given Effort Required in Lifting Load with Trapezoidal Threaded Screw



fx

93) Helix Angle of Screw given Effort Required in Lowering Load with Trapezoidal Threaded Screw

$$lpha = a aniggl(rac{\mathrm{W} \cdot \mu \cdot \mathrm{sec}igl(15 \cdot rac{\pi}{180}igr) - \mathrm{P_{lo}}}{\mathrm{W} + igl(\mathrm{P_{lo}} \cdot \mu \cdot \mathrm{sec}igl(15 \cdot rac{\pi}{180}igr)igr)}igr) igr)$$

$$\mathbf{ex} \left[4.789327^{\circ} = a \tan \left(\frac{1700 \mathrm{N} \cdot 0.15 \cdot \mathrm{sec} \left(15 \cdot \frac{\pi}{180} \right) - 120 \mathrm{N}}{1700 \mathrm{N} + \left(120 \mathrm{N} \cdot 0.15 \cdot \mathrm{sec} \left(15 \cdot \frac{\pi}{180} \right) \right)} \right) \right)$$

94) Helix Angle of Screw given Torque Required in Lifting Load with Trapezoidal Threaded Screw

$$\int \alpha = a \tan \left(\frac{2 \cdot \mathrm{Mt_{li}} - (\mathrm{W} \cdot \mathrm{d_m} \cdot \mu \cdot \mathrm{sec}(0.2618))}{(\mathrm{W} \cdot \mathrm{d_m}) + (2 \cdot \mathrm{Mt_{li}} \cdot \mu \cdot \mathrm{sec}(0.2618))} \right)^{\mathsf{Open Calculator}}$$

ex
$$4.503699^{\circ} = a \tan\left(\frac{2 \cdot 9265 \text{N*mm} - (1700 \text{N} \cdot 46 \text{mm} \cdot 0.15 \cdot \text{sec}(0.2618))}{(1700 \text{N} \cdot 46 \text{mm}) + (2 \cdot 9265 \text{N*mm} \cdot 0.15 \cdot \text{sec}(0.2618))}\right)$$

95) Helix Angle of Screw given Torque Required in Lowering Load with Trapezoidal Threaded Screw

$$\int lpha = a aniggl(rac{(\mathrm{W} \cdot \mathrm{d_m} \cdot \mu \cdot \mathrm{sec}(0.2618)) - (2 \cdot \mathrm{Mt_{lo}})}{(\mathrm{W} \cdot \mathrm{d_m}) + (2 \cdot \mathrm{Mt_{lo}} \cdot \mu \cdot \mathrm{sec}(0.2618))} iggr)$$

Open Calculator 🗗

 $ex \boxed{4.497816^{\circ} = a \tan\left(\frac{(1700 \text{N} \cdot 46 \text{mm} \cdot 0.15 \cdot \sec(0.2618)) - (2 \cdot 2960 \text{N*mm})}{(1700 \text{N} \cdot 46 \text{mm}) + (2 \cdot 2960 \text{N*mm} \cdot 0.15 \cdot \sec(0.2618))}\right)}$



96) Load on Screw given Effort Required in Lifting Load with Trapezoidal Threaded Screw

$$fx W = \frac{P_{li}}{\frac{\mu \cdot \sec((0.2618)) + \tan(\alpha)}{1 - \mu \cdot \sec((0.2618)) \cdot \tan(\alpha)}}$$

$$ex 1697.002N = \frac{402N}{\frac{0.15 \cdot \sec((0.2618)) + \tan(4.5^{\circ})}{1 - 0.15 \cdot \sec((0.2618)) \cdot \tan(4.5^{\circ})}}$$

$$97) \text{ Load on Screw given helix Angle }$$

$$fx W = P_{lo} \cdot \frac{1 + \mu \cdot \sec((0.2618)) \cdot \tan(\alpha)}{(\mu \cdot \sec((0.2618)) - \tan(\alpha))}$$

$$ex 1585.938N = 120N \cdot \frac{1 + 0.15 \cdot \sec((0.2618)) \cdot \tan(4.5^{\circ})}{(0.15 \cdot \sec((0.2618)) - \tan(4.5^{\circ}))}$$

$$98) \text{ Load on Screw given Torque Required in Lifting Load with Trapezoidal Threaded Screw }$$

$$\mathbf{ex} \ 1700.489 \mathrm{N} = 9265 \mathrm{N*mm} \cdot \frac{1 - 0.15 \cdot \mathrm{sec}((0.2618)) \cdot \mathrm{tan}(4.5\degree)}{0.5 \cdot 46 \mathrm{mm} \cdot ((0.15 \cdot \mathrm{sec}((0.2618)) + \mathrm{tan}(4.5\degree)))}$$

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99) Load on Screw given Torque Required in Lowering Load with Trapezoidal Threaded Screw

$$\mathbf{\hat{x}} = \frac{M t_{lo}}{0.5 \cdot d_m \cdot \left(\frac{(\mu \cdot sec((0.2618))) - tan(\alpha)}{1 + (\mu \cdot sec((0.2618)) \cdot tan(\alpha))}\right)}$$

100) Mean Diameter of Screw given Torque in Lifting Load with Trapezoidal Threaded Screw

fx
$$d_{m} = rac{Mt_{li}}{0.5 \cdot W \cdot \left(rac{\mu \cdot sec((0.2618)) + tan(\alpha)}{1 - \mu \cdot sec((0.2618)) \cdot tan(\alpha)}
ight)}$$

$$46.01324 \text{mm} = \frac{9265 \text{N*mm}}{0.5 \cdot 1700 \text{N} \cdot \left(\frac{0.15 \cdot \text{sec}((0.2618)) + \tan(4.5^{\circ})}{1 - 0.15 \cdot \text{sec}((0.2618)) \cdot \tan(4.5^{\circ})}\right)}$$

101) Mean Diameter of Screw given Torque in Lowering Load with Trapezoidal Threaded Screw

$$\begin{aligned} & \textbf{fx} \quad \textbf{d}_{m} = \frac{Mt_{lo}}{0.5 \cdot W \cdot \left(\frac{\mu \cdot \sec((0.2618)) - \tan(\alpha)}{1 + \mu \cdot \sec((0.2618)) \cdot \tan(\alpha)}\right)} \\ & \textbf{ex} \quad \textbf{46.0233mm} = \frac{2960N^{*}mm}{0.5 \cdot 1700N \cdot \left(\frac{0.15 \cdot \sec((0.2618)) - \tan(4.5^{\circ})}{1 + 0.15 \cdot \sec((0.2618)) \cdot \tan(4.5^{\circ})}\right)} \end{aligned}$$



Open Calculator



Open Calculator

102) Torque Required in Lifting Load with Trapezoidal Threaded Screw 🕑

$$9262.334 \text{N*mm} = 0.5 \cdot 46 \text{mm} \cdot 1700 \text{N} \cdot \left(\frac{(0.15 \cdot \sec((0.2618))) + \tan(4.5\degree)}{1 - (0.15 \cdot \sec((0.2618)) \cdot \tan(4.5\degree))}\right)$$

103) Torque Required in Lowering Load with Trapezoidal Threaded Screw 🕑

$$egin{aligned} \mathrm{Mt}_\mathrm{lo} = 0.5 \cdot \mathrm{d}_\mathrm{m} \cdot \mathrm{W} \cdot \left(rac{(\mu \cdot \mathrm{sec}((0.2618))) - \mathrm{tan}(lpha)}{1 + (\mu \cdot \mathrm{sec}((0.2618)) \cdot \mathrm{tan}(lpha))}
ight) \end{aligned}$$

fx

ex

 $2958.501\text{N*mm} = 0.5 \cdot 46\text{mm} \cdot 1700\text{N} \cdot \left(\frac{(0.15 \cdot \sec((0.2618))) - \tan(4.5\degree)}{1 + (0.15 \cdot \sec((0.2618)) \cdot \tan(4.5\degree))}\right)$



Variables Used

- A Bearing area between screw and nut (Square Millimeter)
- d Nominal diameter of screw (Millimeter)
- **d**_c Core diameter of screw (Millimeter)
- D_i Inner Diameter of Collar (Millimeter)
- **d**_m Mean Diameter of Power Screw (*Millimeter*)
- **D**o Outer Diameter of Collar (Millimeter)
- L Lead of Power Screw (Millimeter)
- Mt_{li} Torque for lifting load (Newton Millimeter)
- Mt_{Io} Torque for lowering load (Newton Millimeter)
- Mtt Torsional Moment on Screw (Newton Millimeter)
- **p** Pitch of power screw thread (Millimeter)
- Pli Effort in lifting load (Newton)
- Plo Effort in lowering load (Newton)
- R1 Outer Radius of Power Screw Collar (Millimeter)
- R2 Inner Radius of Power Screw Collar (Millimeter)
- Sb Unit bearing pressure for nut (Newton per Square Millimeter)
- t Thread Thickness (Millimeter)
- T_c Collar Friction Torque for Power Screw (Newton Millimeter)
- tn Transverse shear stress in nut (Newton per Square Millimeter)
- W Load on screw (Newton)
- Wa Axial load on screw (Newton)
- Z Number of Engaged Threads
- α Helix angle of screw (Degree)
- η Efficiency of power screw
- η_{max} Maximum Efficiency of Power Screw

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- µ Coefficient of friction at screw thread
- µcollar Coefficient of Friction for Collar
- σ_c Compressive stress in screw (Newton per Square Millimeter)
- T Torsional shear stress in screw (Newton per Square Millimeter)
- T_S Transverse Shear Stress in Screw (Newton per Square Millimeter)





Constants, Functions, Measurements used

- Constant: pi, 3.14159265358979323846264338327950288 Archimedes' constant
- Function: atan, atan(Number) Inverse tan is used to calculate the angle by applying the tangent ratio of the angle, which is the opposite side divided by the adjacent side of the right triangle.
- Function: sec, sec(Angle) Secant is a trigonometric function that is defined ratio of the hypotenuse to the shorter side adjacent to an acute angle (in a right-angled triangle); the reciprocal of a cosine.
- Function: **sin**, sin(Angle) Sine is a trigonometric function that describes the ratio of the length of the opposite side of a right triangle to the length of the hypotenuse.
- Function: **sqrt**, sqrt(Number) A square root function is a function that takes a non-negative number as an input and returns the square root of the given input number.
- Function: tan, tan(Angle)
 The tangent of an angle is a trigonometric ratio of the length of the side opposite an angle to the length of the side adjacent to an angle in a right triangle.
- Measurement: Length in Millimeter (mm) Length Unit Conversion
- Measurement: Area in Square Millimeter (mm²) Area Unit Conversion
- Measurement: Pressure in Newton per Square Millimeter (N/mm²) Pressure Unit Conversion
- Measurement: Force in Newton (N) Force Unit Conversion
- Measurement: Angle in Degree (°) Angle Unit Conversion
- Measurement: Torque in Newton Millimeter (N*mm) Torque Unit Conversion



• Measurement: Stress in Newton per Square Millimeter (N/mm²) Stress Unit Conversion





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Refrigeration and Air Conditioning
 Formulas

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