



Design of Pressure Vessels Formulas

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List of 52 Design of Pressure Vessels Formulas

Design of Pressure Vessels @

Bernie's and Clavarino's Equation

1) Inner Diameter of Pressurized Cylinder from Bernie's Equation

$$\boxed{\mathbf{fx}} d_i = \frac{2 \cdot t_w}{\left(\left(\frac{\sigma_t + ((1 - (\mathbf{v}) \cdot P_i))}{\sigma_t - ((1 + \mathbf{v}) \cdot P_i)} \right)^{0.5} \right) - 1}$$

2) Inner Diameter of Pressurized Cylinder from Clavarino's Equation

$$\boxed{\mathbf{d}_i = \frac{2 \cdot t_w}{\left(\left(\frac{\sigma_t + ((1 - (2 \cdot \nu) \cdot P_i))}{\sigma_t - ((1 + \nu) \cdot P_i)}\right)^{0.5}\right) - 1}}$$

3) Thickness of Pressurized Cylinder from Bernie's Equation ${\ensuremath{ \mbox{\cite{C}}}}$

$$t_w = \left(\frac{d_i}{2}\right) \cdot \left(\left(\left(\frac{\sigma_t + ((1 - (\textbf{v}) \cdot P_i))}{\sigma_t - ((1 + \textbf{v}) \cdot P_i)}\right)^{0.5}\right) - 1 \right)$$

$$\boxed{ 18.47176 \mathrm{mm} = \left(\frac{465 \mathrm{mm}}{2} \right) \cdot \left(\left(\left(\frac{75 \mathrm{N/mm^2} + ((1 - (0.3) \cdot 10.2 \mathrm{MPa}))}{75 \mathrm{N/mm^2} - ((1 + 0.3) \cdot 10.2 \mathrm{MPa})} \right)^{0.5} \right) - 1 \right) }$$



4) Thickness of Pressurized Cylinder from Clavarino's Equation 🗗

 $\boxed{\mathbf{f}_{w}} = \left(\frac{d_{i}}{2}\right) \cdot \left(\left(\left(\frac{\sigma_{t} + \left(\left(1 - \left(2 \cdot \boldsymbol{\nu}\right) \cdot P_{i}\right)\right)}{\sigma_{t} - \left(\left(1 + \boldsymbol{\nu}\right) \cdot P_{i}\right)}\right)^{0.5}\right) - 1\right)$

Open Calculator 🗗

$$\boxed{ 13.07617 \mathrm{mm} = \left(\frac{465 \mathrm{mm}}{2} \right) \cdot \left(\left(\left(\frac{75 \mathrm{N/mm^2} + ((1 - (2 \cdot 0.3) \cdot 10.2 \mathrm{MPa}))}{75 \mathrm{N/mm^2} - ((1 + 0.3) \cdot 10.2 \mathrm{MPa})} \right)^{0.5} \right) - 1 \right) }$$

Bolt of Pressurized Cylinder

5) Change in External Load due to Pressure Inside Cylinder given kb and kc

 $\Delta P_{\mathrm{i}} = P_{\mathrm{ext}} \cdot \left(rac{k_{\mathrm{b}}}{k_{\mathrm{c}} + k_{\mathrm{b}}}
ight)$

Open Calculator

$$= 5193.662 N = 25000 N \cdot \left(\frac{1180 kN/mm}{4500 kN/mm + 1180 kN/mm} \right)$$

6) Change in External Load on Bolt due to Pressure Inside Cylinder

 $\Delta P_{
m i} = P_{
m b} - P_{
m l}$ = 4500 N = 24500 N - 20000 N

Open Calculator 🗗

- 7) Decrease in Outer Diameter of Cylinder given Total deformation in Pressure Vessel
- fx $\delta_{
 m c} = \delta \delta_{
 m j}$

Open Calculator 🚰

- 0.8 mm = 1.20 mm 0.4 mm
- 8) External Load on Bolt due to Internal Pressure given kb and kc

$$ext{P}_{ ext{ext}} = \Delta ext{P}_{ ext{i}} \cdot \left(rac{ ext{k}_{ ext{c}} + ext{k}_{ ext{b}}}{ ext{k}_{ ext{b}}}
ight)$$

Open Calculator

$$oxed{ex} 24308.47 ext{N} = 5050 ext{N} \cdot \left(rac{4500 ext{kN/mm} + 1180 ext{kN/mm}}{1180 ext{kN/mm}}
ight)^{-1}$$



9) Initial Preload due to Bolt tightening 🗗

fx
$$P_l = P_b - \Delta P_i$$

Open Calculator 🗗

$$| | 19450N = 24500N - 5050N |$$

10) Initial Preload due to Bolt tightening given kb and kc

$$P_{l} = P_{max} \cdot \left(rac{k_{b}}{k_{c} + k_{b}}
ight)$$

$$\boxed{ 5235.211 \mathrm{N} = 25200 \mathrm{N} \cdot \left(\frac{1180 \mathrm{kN/mm}}{4500 \mathrm{kN/mm} + 1180 \mathrm{kN/mm}} \right) }$$

11) Internal Diameter of Pressurized Cylinder

$$d_i = 2 \cdot rac{t_w}{\left(\left(rac{\sigma_t + P_i}{\sigma_t - P_i}
ight)^{rac{1}{2}}
ight) - 1}$$

$$\boxed{ \begin{array}{c} \textbf{ex} \\ 409.1269 mm = 2 \cdot \frac{30 mm}{\left(\left(\frac{75 N/mm^2 + 10.2 MPa}{75 N/mm^2 - 10.2 MPa} \right)^{\frac{1}{2}} \right) - 1 } \\ \end{array} }$$

12) Maximum Load inside Pressurized Cylinder when Joint is on verge of opening

$$ext{P}_{ ext{max}} = ext{P}_1 \cdot \left(rac{ ext{k}_{ ext{c}} + ext{k}_{ ext{b}}}{ ext{k}_{ ext{b}}}
ight)$$

$$= 96271.19 \text{N} = 20000 \text{N} \cdot \left(\frac{4500 \text{kN/mm} + 1180 \text{kN/mm}}{1180 \text{kN/mm}} \right)$$

13) Resultant Load on Bolt given Pre load

fx
$$P_{b}=P_{l}+\Delta P_{i}$$

$$25050 \mathrm{N} = 20000 \mathrm{N} + 5050 \mathrm{N}$$



14) Thickness of Pressurized Cylinder 🗗

$$\mathbf{f}_{\mathrm{w}} = \left(rac{d_{\mathrm{i}}}{2}
ight) \cdot \left(\left(\left(rac{\sigma_{\mathrm{t}} + P_{\mathrm{i}}}{\sigma_{\mathrm{t}} - P_{\mathrm{i}}}
ight)^{rac{1}{2}}
ight) - 1
ight)$$

Gasket Joint

15) Approximate Stiffness of Cylinder Cover, Cylinder Flange and Gasket

$$\mathbf{K} = \left(2 \cdot \pi \cdot \left(\mathrm{d}^2
ight)
ight) \cdot \left(rac{\mathrm{E}}{\mathrm{t}}
ight)$$

$$= \sum_{i=1}^{n} 5089.38 \text{kN/mm} = \left(2 \cdot \pi \cdot \left((15 \text{mm})^2 \right) \right) \cdot \left(\frac{90000 \text{N/mm}^2}{25 \text{mm}} \right)$$

16) Combined Stiffness of Cylinder Cover, Cylinder Flange and Gasket

$$\mathbf{k}_{\mathrm{c}} = rac{1}{\left(rac{1}{\mathrm{k}_{1}}
ight) + \left(rac{1}{\mathrm{k}_{2}}
ight) + \left(rac{1}{\mathrm{k}_{\mathrm{g}}}
ight)}$$

$$\boxed{ 4721.105 \text{kN/mm} = \frac{1}{\left(\frac{1}{10050 \text{kN/mm}}\right) + \left(\frac{1}{11100 \text{kN/mm}}\right) + \left(\frac{1}{45000 \text{kN/mm}}\right) } }$$

17) Increase in Inner Diameter of Jacket given Total deformation of Pressure Vessel

fx
$$\delta_{
m j} = \delta - \delta_{
m c}$$

$$0.4 \text{mm} = 1.20 \text{mm} - 0.80 \text{mm}$$

18) Nominal Diameter of Gasket Joint

$$\mathbf{f}$$
 $\mathbf{d} = \sqrt{\mathbf{K} \cdot rac{\mathbf{t}}{2 \cdot \pi \cdot \mathbf{E}}}$

$$= \sqrt{5090 \text{kN/mm} \cdot \frac{25 \text{mm}}{2 \cdot \pi \cdot 90000 \text{N/mm}^2} }$$

19) Nominal Diameter of Gasket Joint Bolt given Stiffness, total thickness and Young's Modulus

$$\mathrm{fc} \left[\mathrm{d} = \sqrt{\mathrm{k_b} \cdot 4 \cdot rac{\mathrm{l}}{\pi \cdot \mathrm{E}}}
ight]$$

ex
$$30.30094 \text{mm} = \sqrt{1180 \text{kN/mm} \cdot 4 \cdot \frac{55 \text{mm}}{\pi \cdot 90000 \text{N/mm}^2}}$$

20) Stiffness of Bolt of Gasket Joint given Nominal Diameter, Total Thickness, and Young's Modulus

$$\mathbf{k}_{\mathrm{b}} = \left(\pi \cdot rac{\mathrm{d}^2}{4}
ight) \cdot \left(rac{\mathrm{E}}{\mathrm{l}}
ight)$$

ex
$$289.1693 \text{kN/mm} = \left(\pi \cdot \frac{(15 \text{mm})^2}{4}\right) \cdot \left(\frac{90000 \text{N/mm}^2}{55 \text{mm}}\right)$$

21) Stiffness of Cylinder Cover of Gasket Joint

$$\mathbf{k}_1 = rac{1}{\left(rac{1}{\mathrm{k_c}}
ight) - \left(\left(rac{1}{\mathrm{k_2}}
ight) + \left(rac{1}{\mathrm{k_g}}
ight)
ight)}$$

$$= \frac{1}{\left(\frac{1}{4500 \text{kN/mm}}\right) - \left(\left(\frac{1}{11100 \text{kN/mm}}\right) + \left(\frac{1}{45000 \text{kN/mm}}\right)\right)}$$



22) Stiffness of Cylinder Flange of Gasket Joint 🚰

$$\mathbf{k}_2 = rac{1}{\left(rac{1}{\mathrm{k_c}}
ight) - \left(\left(rac{1}{\mathrm{k_1}}
ight) + \left(rac{1}{\mathrm{k_g}}
ight)
ight)}$$

Open Calculator 🗗

$$= \frac{1}{\left(\frac{1}{4500 \text{kN/mm}}\right) - \left(\left(\frac{1}{10050 \text{kN/mm}}\right) + \left(\frac{1}{45000 \text{kN/mm}}\right)\right)}$$

23) Stiffness of Gasket of Gasket Joint

$$k_{\mathrm{g}} = rac{1}{\left(rac{1}{k_{\mathrm{c}}}
ight) - \left(\left(rac{1}{k_{1}}
ight) + \left(rac{1}{k_{2}}
ight)
ight)}$$

Open Calculator

$$= \frac{1}{\left(\frac{1}{4500 \text{kN/mm}}\right) - \left(\left(\frac{1}{10050 \text{kN/mm}}\right) + \left(\frac{1}{11100 \text{kN/mm}}\right)\right)}$$

24) Thickness of Member under Compression for Gasket Joint

$$\mathbf{t} = \left(\pi \cdot \frac{\mathrm{d}^2}{4}\right) \cdot \left(\frac{\mathrm{E}}{\mathrm{K}}\right)$$

Open Calculator

25) Total Deformation of Pressure Vessel given Increase in Inner Diameter of Jacket 💪

fx
$$\delta = \delta_{
m j} + \delta_{
m c}$$

Open Calculator

$$1.2 \text{mm} = 0.4 \text{mm} + 0.80 \text{mm}$$

$$\mathbf{f}$$
 $\mathbf{l} = \left(\pi \cdot rac{\mathrm{d}^2}{4}
ight) \cdot \left(rac{\mathrm{E}}{\mathrm{k_b}}
ight)$

Open Calculator 🗗

$$= \left(\pi \cdot \frac{(15 \mathrm{mm})^2}{4}\right) \cdot \left(\frac{90000 \mathrm{N/mm^2}}{1180 \mathrm{kN/mm}}\right)^2$$





27) Young's Modulus of Gasket Joint 🚰

 $\mathbf{E} = 4 \cdot \mathbf{K} \cdot rac{\mathrm{t}}{\pi \cdot (\mathrm{d}^2)}$

Open Calculator 🗗

28) Young's Modulus of Gasket Joint given Stiffness, Total Thickness and Nominal Diameter

$$\mathbf{E} = \mathbf{k}_{\mathrm{b}} \cdot rac{1}{\pi \cdot rac{\mathrm{d}^2}{4}}$$

Open Calculator 🚰

$$= \frac{367258.9 \text{N/mm}^2 = 1180 \text{kN/mm} \cdot \frac{55 \text{mm}}{\pi \cdot \frac{(15 \text{mm})^2}{4}} }$$

Thick Cylinder Vessel

29) External Pressure acting on Thick Cylinder given Radial Stress

 $\mathbf{fx} egin{equation} \mathbf{P}_{\mathrm{o}} = rac{\sigma_{\mathrm{r}}}{\left(rac{\mathrm{d}_{\mathrm{o}}^2}{\left(\mathrm{d}_{\mathrm{o}}^2
ight) - \left(\mathrm{d}_{\mathrm{i}}^2
ight)}
ight) \cdot \left(\left(rac{\mathrm{d}_{\mathrm{i}}^2}{4 \cdot \left(\mathrm{r}^2
ight)}
ight) + 1
ight)} \end{split}$

Open Calculator 🗗

$$11.77034 \text{MPa} = \frac{80 \text{N/mm}^2}{\left(\frac{(550 \text{mm})^2}{\left((550 \text{mm})^2\right) - \left((465 \text{mm})^2\right)}\right) \cdot \left(\left(\frac{(465 \text{mm})^2}{4 \cdot \left((240 \text{mm})^2\right)}\right) + 1\right)}$$

30) External Pressure acting on Thick Cylinder given Tangential Stress

$$P_{\mathrm{o}} = rac{\sigma_{\mathrm{tang}}}{\left(rac{d_{\mathrm{o}}^2}{\left(d_{\mathrm{o}}^2) - \left(d_{\mathrm{i}}^2
ight)}
ight) \cdot \left(\left(rac{d_{\mathrm{i}}^2}{4 \cdot (\mathrm{r}^2)}
ight) + 1
ight)}$$

Open Calculator 🗗

$$7.062204 \text{MPa} = \frac{48 \text{N/mm}^2}{\left(\frac{(550 \text{mm})^2}{\left((550 \text{mm})^2\right) - \left((465 \text{mm})^2\right)}\right) \cdot \left(\left(\frac{(465 \text{mm})^2}{4 \cdot \left((240 \text{mm})^2\right)}\right) + 1\right)}$$





31) Internal Pressure in Thick Cylinder given Longitudinal Stress 🗗

$$ext{P}_{i} = \sigma_{l} \cdot rac{\left(d_{o}^{2}
ight) - \left(d_{i}^{2}
ight)}{d_{i}^{2}}$$

32) Internal Pressure in Thick Cylinder given Radial Stress

$$\Pr_i = \frac{\sigma_r}{\left(\frac{d_i^2}{\left(d_o^2\right) - \left(d_i^2\right)}\right) \cdot \left(\left(\frac{d_o^2}{4 \cdot (r^2)}\right) + 1\right)}$$

$$= \frac{80 \text{N/mm}^2}{\left(\frac{(465 \text{mm})^2}{\left((550 \text{mm})^2\right) - \left((465 \text{mm})^2\right)}\right) \cdot \left(\left(\frac{(550 \text{mm})^2}{4 \cdot \left((240 \text{mm})^2\right)}\right) + 1\right)}$$

33) Internal Pressure in Thick Cylinder given Tangential Stress

$$P_i = rac{\sigma_{tang}}{\left(rac{d_i^2}{\left(d_o^2
ight) - \left(d_i^2
ight)}
ight) \cdot \left(\left(rac{d_o^2}{4 \cdot (r^2)}
ight) + 1
ight)}$$

$$8.280509 MPa = \frac{48 N/mm^2}{\left(\frac{(465 mm)^2}{\left((550 mm)^2\right) - \left((465 mm)^2\right)}\right) \cdot \left(\left(\frac{(550 mm)^2}{4 \cdot \left((240 mm)^2\right)}\right) + 1\right)}$$

34) Longitudinal Stress in Thick Cylinder subjected to Internal Pressure

$$\sigma_{l} = \left(P_{i} \cdot rac{d_{i}^{2}}{\left(d_{o}^{2}
ight) - \left(d_{i}^{2}
ight)}
ight)$$





35) Radial Stress in Thick Cylinder subjected to External Pressure 🗹

 $\sigma_{
m r} = \left(P_{
m o} \cdot rac{d_{
m o}^2}{\left(d_{
m o}^2
ight) - \left(d_{
m i}^2
ight)}
ight) \cdot \left(1 - \left(rac{d_{
m i}^2}{4 \cdot ({
m r}^2)}
ight)
ight)$

Open Calculator

 $\boxed{ 1.725723 \text{N/mm}^2 = \left(8 \text{MPa} \cdot \frac{\left(550 \text{mm} \right)^2}{\left(\left(550 \text{mm} \right)^2 \right) - \left(\left(465 \text{mm} \right)^2 \right)} \right) \cdot \left(1 - \left(\frac{\left(465 \text{mm} \right)^2}{4 \cdot \left(\left(240 \text{mm} \right)^2 \right)} \right) \right) }$

36) Radial Stress in Thick Cylinder subjected to Internal Pressure

 $\sigma_{
m r} = \left(P_{
m i} \cdot rac{d_{
m i}^2}{\left(d_{
m o}^2
ight) - \left(d_{
m i}^2
ight)}
ight) \cdot \left(\left(rac{d_{
m o}^2}{4 \cdot ({
m r}^2)}
ight) - 1
ight)$

Open Calculator

ex

 $oxed{7.999704 ext{N/mm}^2 = \left(10.2 ext{MPa} \cdot rac{\left(465 ext{mm}
ight)^2}{\left(\left(550 ext{mm}
ight)^2
ight) - \left(\left(465 ext{mm}
ight)^2
ight)}
ight) \cdot \left(\left(rac{\left(550 ext{mm}
ight)^2}{4 \cdot \left(\left(240 ext{mm}
ight)^2
ight)}
ight) - 1
ight)}$

37) Tangential Stress in Thick Cylinder subjected to External Pressure

 $\sigma_{ ext{tang}} = \left(\mathrm{P_o} \cdot rac{\mathrm{d_o^2}}{\left(\mathrm{d_o^2}
ight) - \left(\mathrm{d_i^2}
ight)}
ight) \cdot \left(\left(rac{\mathrm{d_i^2}}{4 \cdot (\mathrm{r^2})}
ight) + 1
ight)$

Open Calculator

 $= \left(8\text{MPa} \cdot \frac{\left(550\text{mm}\right)^2}{\left(\left(550\text{mm}\right)^2 \right) - \left(\left(465\text{mm}\right)^2 \right)} \right) \cdot \left(\left(\frac{\left(465\text{mm}\right)^2}{4 \cdot \left(\left(240\text{mm}\right)^2 \right)} \right) + 1 \right)$

38) Tangential Stress in Thick Cylinder subjected to Internal Pressure

 $\sigma_{
m tang} = \left(\mathrm{P_i} \cdot rac{\mathrm{d_i^2}}{\left(\mathrm{d_o^2}
ight) - \left(\mathrm{d_i^2}
ight)}
ight) \cdot \left(\left(rac{\mathrm{d_o^2}}{4 \cdot (\mathrm{r^2})}
ight) + 1
ight)^2$

Open Calculator 🚰

ex

 $\boxed{59.1268 \text{N/mm}^2 = \left(10.2 \text{MPa} \cdot \frac{\left(465 \text{mm}\right)^2}{\left(\left(550 \text{mm}\right)^2\right) - \left(\left(465 \text{mm}\right)^2\right)}\right) \cdot \left(\left(\frac{\left(550 \text{mm}\right)^2}{4 \cdot \left(\left(240 \text{mm}\right)^2\right)}\right) + 1\right)}$





Thin Cylinder Vessel 2

 $\mathbf{f}_{\mathrm{w}} = \mathrm{P}_{\mathrm{i}} \cdot rac{\mathrm{d}_{\mathrm{i}}}{4 \cdot \sigma_{\mathrm{l}}}$

39) Cylinder Wall Thickness of Thin Cylinder given Longitudinal Stress 🖸

ex 17.4375mm = 10.2MPa $\cdot \frac{465$ mm $\cdot \frac{465$ mm}{4 $\cdot \frac{68}{100}$ MPa}

Open Calculator 🗗

40) Cylinder Wall Thickness of Thin Cylinder given Tangential Stress

 $\boxed{\textbf{fx}} t_w = P_i \cdot \frac{d_i}{2 \cdot \sigma_{tang}}$

Open Calculator 🗗

 $2 \cdot \sigma_{ ext{tang}}$

 $oxed{49.40625 ext{mm}} = 10.2 ext{MPa} \cdot rac{465 ext{mm}}{2 \cdot 48 ext{N/mm}^2}$

41) Inner Diameter of Thin Cylinder given Longitudinal Stress 🗗

 $d_i = 4 \cdot t_w \cdot rac{\sigma_l}{P_i}$

Open Calculator 🗗

Open Calculator 2

 $800 \mathrm{mm} = 4 \cdot 30 \mathrm{mm} \cdot \frac{68 \mathrm{N/mm^2}}{10.2 \mathrm{MPa}}$

42) Inner Diameter of Thin Cylinder given Tangential Stress

 $d_{i} = 2 \cdot t_{w} \cdot rac{\sigma_{tang}}{P_{i}}$

1633

ex $282.3529 \mathrm{mm} = 2 \cdot 30 \mathrm{mm} \cdot \frac{48 \mathrm{N/mm^2}}{10.2 \mathrm{MPa}}$

43) Inner Diameter of Thin Spherical Shell given Permissible Tensile Stress

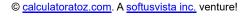
 $d_i = 4 \cdot t_w \cdot rac{\sigma_t}{P_i}$

Open Calculator

 $oxed{ex}882.3529 \mathrm{mm} = 4 \cdot 30 \mathrm{mm} \cdot rac{75 \mathrm{N/mm^2}}{10.2 \mathrm{MPa}}$









44) Inner Diameter of Thin Spherical Shell given Volume

$$\mathbf{f}$$
 $\mathbf{d}_{i} = \left(6 \cdot rac{V}{\pi}
ight)^{rac{1}{3}}$

Open Calculator

$$781.5926 \text{mm} = \left(6 \cdot \frac{0.25 \text{m}^3}{\pi}\right)^{\frac{1}{3}}$$

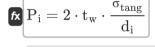
45) Internal Pressure in Thin Cylinder given Longitudinal Stress

$$\boxed{\mathbf{fx}} P_i = 4 \cdot t_w \cdot \frac{\sigma_l}{d_i}$$

Open Calculator

ex
$$17.54839 \text{MPa} = 4 \cdot 30 \text{mm} \cdot \frac{68 \text{N/mm}^2}{465 \text{mm}}$$

46) Internal Pressure in Thin Cylinder given Tangential Stress



Open Calculator

$= 2 \cdot 30 \text{mm} \cdot \frac{48 \text{N/mm}^2}{465 \text{mm}}$

47) Internal Pressure in Thin Spherical Shell given Permissible Tensile Stress

$$P_i = 4 \cdot t_w \cdot rac{\sigma_t}{d_i}$$

Open Calculator

ex
$$19.35484 \text{MPa} = 4 \cdot 30 \text{mm} \cdot \frac{75 \text{N/mm}^2}{465 \text{mm}}$$

48) Longitudinal Stress in Thin Cylinder given Internal Pressure

$$\sigma_l = P_i \cdot rac{d_i}{4 \cdot t_w}$$

Open Calculator



49) Permissible Tensile Stress in Thin Spherical Shell

$$\sigma_{
m t} = P_{
m i} \cdot rac{d_{
m i}}{4 \cdot t_{
m err}}$$

Open Calculator

$$\label{eq:second} \boxed{39.525 N/mm^2 = 10.2 MPa \cdot \frac{465 mm}{4 \cdot 30 mm}}$$

50) Tangential Stress in Thin Cylinder given Internal Pressure

$$\sigma_{tang} = P_i \cdot rac{d_i}{2 \cdot t_w}$$

Open Calculator 🚰

$$ext{ex} 79.05 ext{N/mm}^2 = 10.2 ext{MPa} \cdot rac{465 ext{mm}}{2 \cdot 30 ext{mm}}$$

51) Thickness of Thin Spherical Shell given Permissible tensile stress

$$\mathbf{f}\mathbf{x}egin{bmatrix} \mathbf{t}_{w} = P_{i} \cdot rac{d_{i}}{4 \cdot \sigma_{t}} \end{bmatrix}$$

Open Calculator 🚰

ex
$$15.81 \text{mm} = 10.2 \text{MPa} \cdot \frac{465 \text{mm}}{4 \cdot 75 \text{N/mm}^2}$$

52) Volume of Thin Spherical Shell given Inner Diameter

$$V = \pi \cdot rac{d_{
m i}^3}{6}$$

fx
$$V=\pi\cdotrac{d_i^3}{6}$$
 ex $0.052645 ext{m}^3=\pi\cdotrac{(465 ext{mm})^3}{6}$



Variables Used

- **d** Nominal Bolt Diameter on Cylinder (Millimeter)
- d; Inner Diameter of Pressurized Cylinder (Millimeter)
- do Outer Diameter of Pressurized Cylinder (Millimeter)
- E Modulus of Elasticity for Gasket Joint (Newton per Square Millimeter)
- **K** Approximate Stiffness of Gasketed Joint (Kilonewton per Millimeter)
- **k**₁ Stiffness of Pressurized Cylinder Cover (Kilonewton per Millimeter)
- k₂ Stiffness of Pressurized Cylinder Flange (Kilonewton per Millimeter)
- **k**_b Stiffness of Pressurized Cylinder Bolt (Kilonewton per Millimeter)
- **k**_C Combined Stiffness for Gasket Joint (Kilonewton per Millimeter)
- k_a Stiffness of Gasket (Kilonewton per Millimeter)
- I Total Thickness of parts held together by Bolt (Millimeter)
- Pb Resultant Load on Pressurized Cylinder Bolt (Newton)
- Pext External Load on Pressurized Cylinder Bolt (Newton)
- Pi Internal Pressure on Cylinder (Megapascal)
- P_I Initial Preload Due to Bolt Tightening (Newton)
- Pmax Maximum Force Inside Pressurized Cylinder (Newton)
- P_o External Pressure on Cylinder (Megapascal)
- r Radius of pressurized cylinder (Millimeter)
- t Thickness of Member under Compression (Millimeter)
- t_w Thickness of Pressurized Cylinder Wall (Millimeter)
- V Volume of Thin Spherical Shell (Cubic Meter)
- δ Total Deformation of Pressure Vessel (Millimeter)
- δ_c Decrease in Outer Diameter of Cylinder (Millimeter)
- δ_i Increase in Inner Diameter of Jacket (Millimeter)
- ΔP_i Increase in Bolt Load of Cylinder (Newton)
- σ_I Longitudinal Stress in Pressurized Cylinder (Newton per Square Millimeter)
- σ_r Radial Stress in Pressurized Cylinder (Newton per Square Millimeter)
- σ_t Permissible Tensile Stress in Pressurized Cylinder (Newton per Square Millimeter)
- σ_{tang} Tangential Stress in Pressurized Cylinder (Newton per Square Millimeter)





• ν Poisson's Ratio of Pressurized Cylinder





Constants, Functions, Measurements used

- Constant: pi, 3.14159265358979323846264338327950288
 Archimedes' constant
- Function: sqrt, sqrt(Number)

A square root function is a function that takes a non-negative number as an input and returns the square root of the given input number.

- Measurement: Length in Millimeter (mm)
 Length Unit Conversion
- Measurement: Volume in Cubic Meter (m³)

 Volume Unit Conversion
- Measurement: Pressure in Megapascal (MPa)

 Pressure Unit Conversion
- Measurement: Force in Newton (N)
 Force Unit Conversion
- Measurement: Stiffness Constant in Kilonewton per Millimeter (kN/mm)
 Stiffness Constant Unit Conversion
- Measurement: Stress in Newton per Square Millimeter (N/mm²)

 Stress Unit Conversion





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